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# Wood transverse compression using hyperelastic plastic behavior simulated in the Material Point Method (MPM)

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# Outline

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- Hyperelastic-plastic model
- Validation of the model
- Application to wood transverse compression

# Hyper elastic-plastic model

- Objective: To simulate large elastic deformations involving plastic behavior that are seen in materials such as wood, composites, etc.
- The model uses a multiplicative decomposition of the deformation gradient.

$$\underline{\underline{\mathbf{F}}} = \underline{\underline{\mathbf{F}}^e} \cdot \underline{\underline{\mathbf{F}}^p}$$

- The stress-strain law derives from a stored energy, the Neo-Hookean potential was considered,

$$W = \frac{1}{2} \kappa \left[ \frac{1}{2} (J^{e^2} - 1) - \ln J^e \right] + \frac{1}{2} \mu \left[ \text{tr}(\underline{\underline{\mathbf{b}}^e}) - 3 \right]$$

- The plastic behavior is handled by a plastic flow condition
  - Mises-Huber classical condition - Isotropic hardening

$$f(\underline{\underline{\boldsymbol{\tau}}}, \alpha) = \|\underline{\underline{\boldsymbol{\tau}}^d}\| - \sqrt{\frac{2}{3}} \left[ \sigma_Y + K(\alpha) \right]$$

# Hyper elastic-plastic model - cont'd

- Stress-strain elastic constitutive law

$$\begin{cases} \underline{\underline{\tau}} = J^e p \underline{\underline{1}} + \mu \operatorname{dev} \left[ \underline{\underline{B}}^e \right] \\ p = U'(J^e) = \kappa (J^{e2} - 1) / J^e \end{cases}$$

- Associate flow rule and plastic cumulative strain rate

$$\begin{cases} L v(\underline{\underline{B}}^e) = \underline{\underline{F}}^{-1} \cdot \frac{\partial}{\partial t} \left( \underline{\underline{C}}^{p-1} \right) \cdot \underline{\underline{F}}^{-T} = -\frac{2}{3} \lambda \operatorname{tr}(\underline{\underline{B}}^e) \underline{\underline{n}} \cdot \underline{\underline{F}}^{-T} \quad \text{with} \quad \underline{\underline{n}} = \underline{\underline{\tau}}^d / \left\| \underline{\underline{\tau}}^d \right\| \\ \alpha = \sqrt{\frac{2}{3}} \lambda \end{cases}$$

- Implemented in Explicit MPM software NairnMPM
  - In NairnMPM, specific Cauchy stress is needed

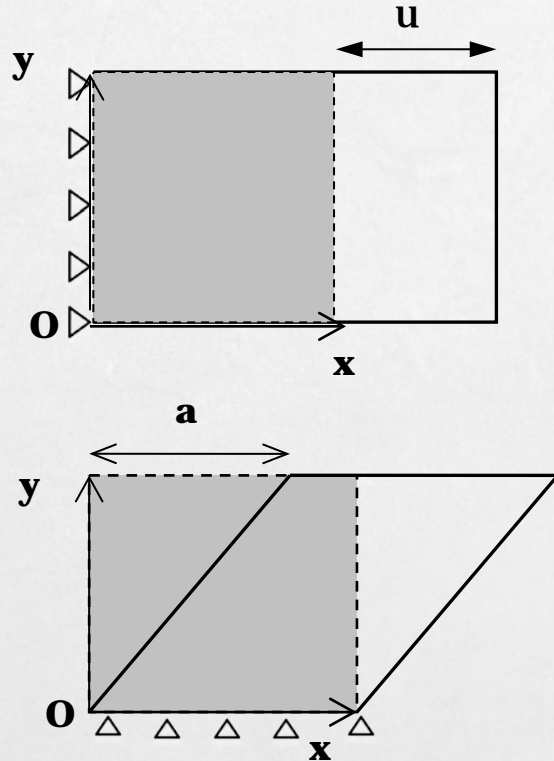
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# Numerical validations

- Tensile and shear elementary tests

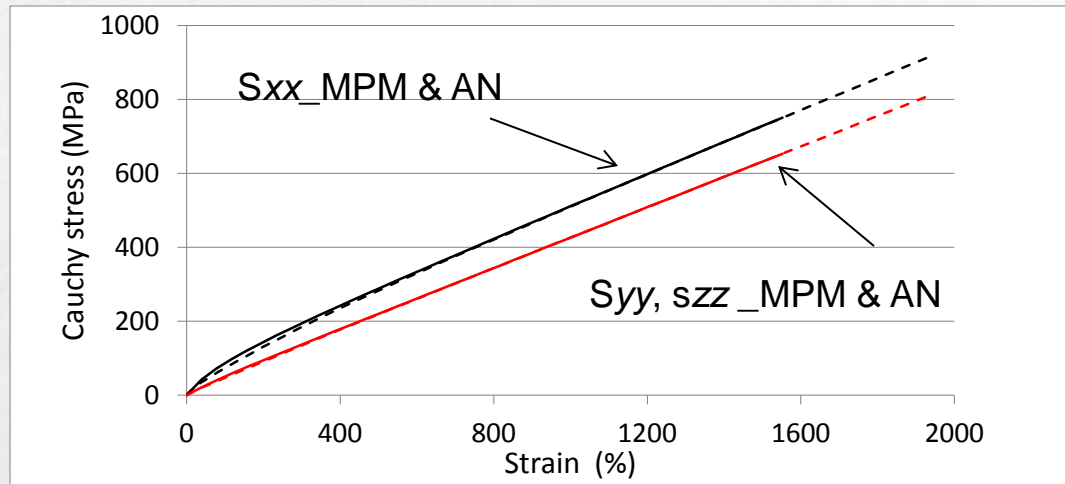
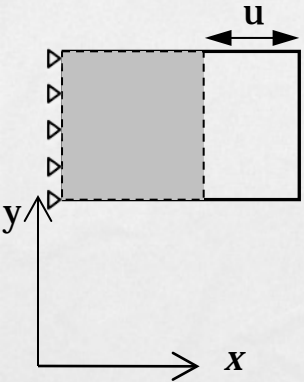


- Isotropic material  
 $E = 100 \text{ MPa}$ ,  $\nu = 0.4$   
 $\rho = 1 \text{ g/cm}^3$   
 $\sigma_Y = 100 \text{ MPa}$ ,  $E_p = 0 \text{ MPa}$

- All simulations are 2D plane strain

# Elementary tests

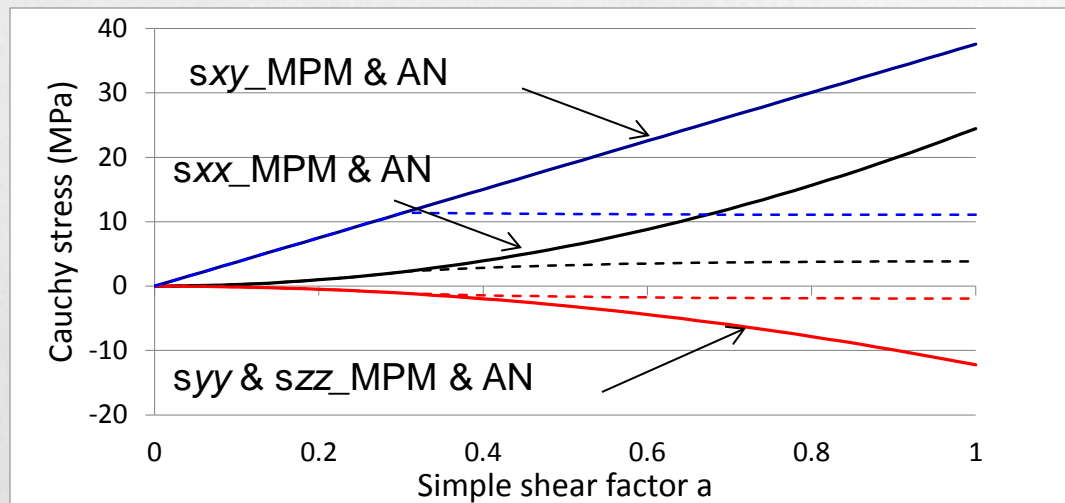
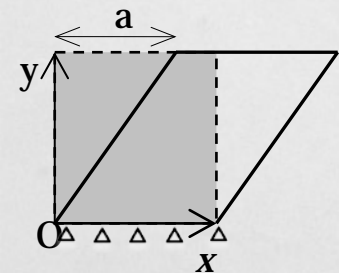
- Restrained Tensile Test



**More than  
2000% of  
strain**

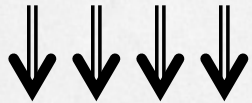
(using CPDI)

- Simple Shear Test



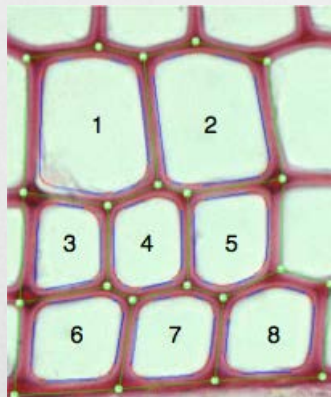
# Numerical validations

- Compression test on a cellular material sample



- Polyoxymethylene (POM)  
 $E = 3100 \text{ MPa}$ ,  $\nu = 0.4$   
 $\rho = 1.4 \text{ g / cm}^3$   
 $\sigma_Y = 72 \text{ MPa}$ ,  $E_p = 0 \text{ MPa}$

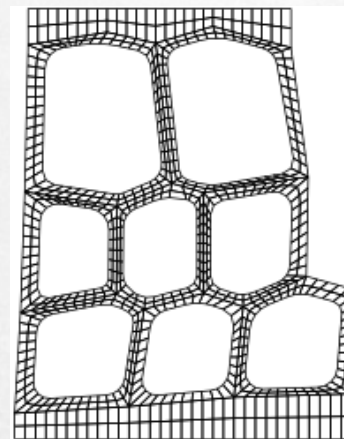
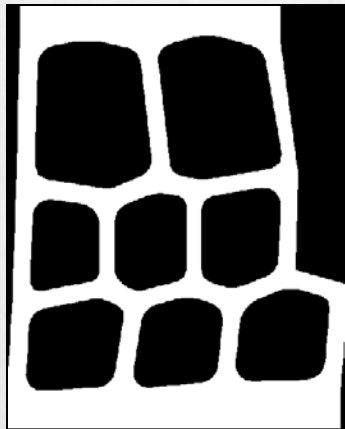
- Image of a cross-section of soft wood anatomy with 8 selected cells





# Cellular material sample

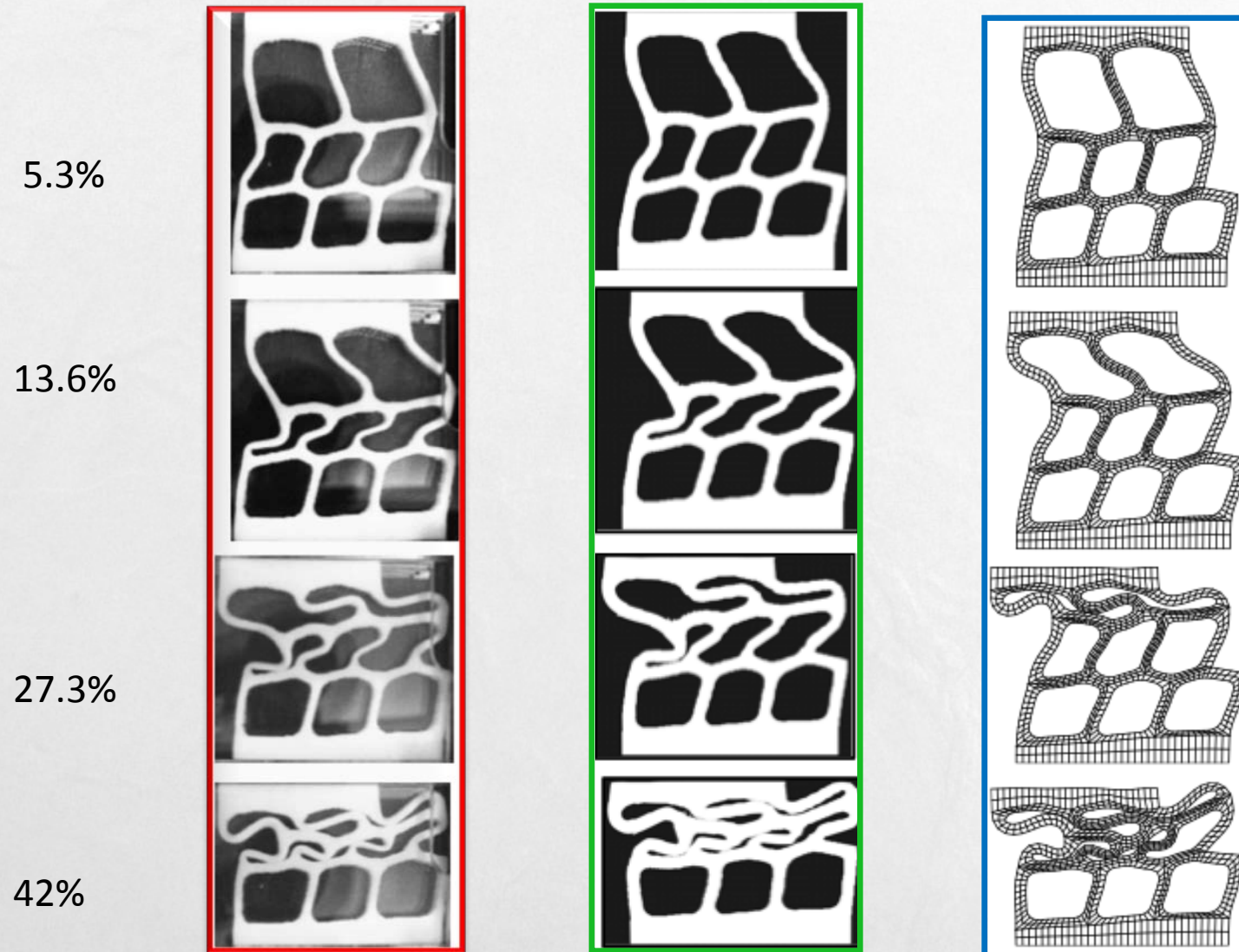
- MPM and finite elements discretization



- Micrograph Area :  $0.832 \times 0.541 \text{ mm}^2$
  - MPM Grid discretization:  $300 \times 194$  elements
  - Number of particles : 47114
  - Res: 300 ppp
- FEM mesh

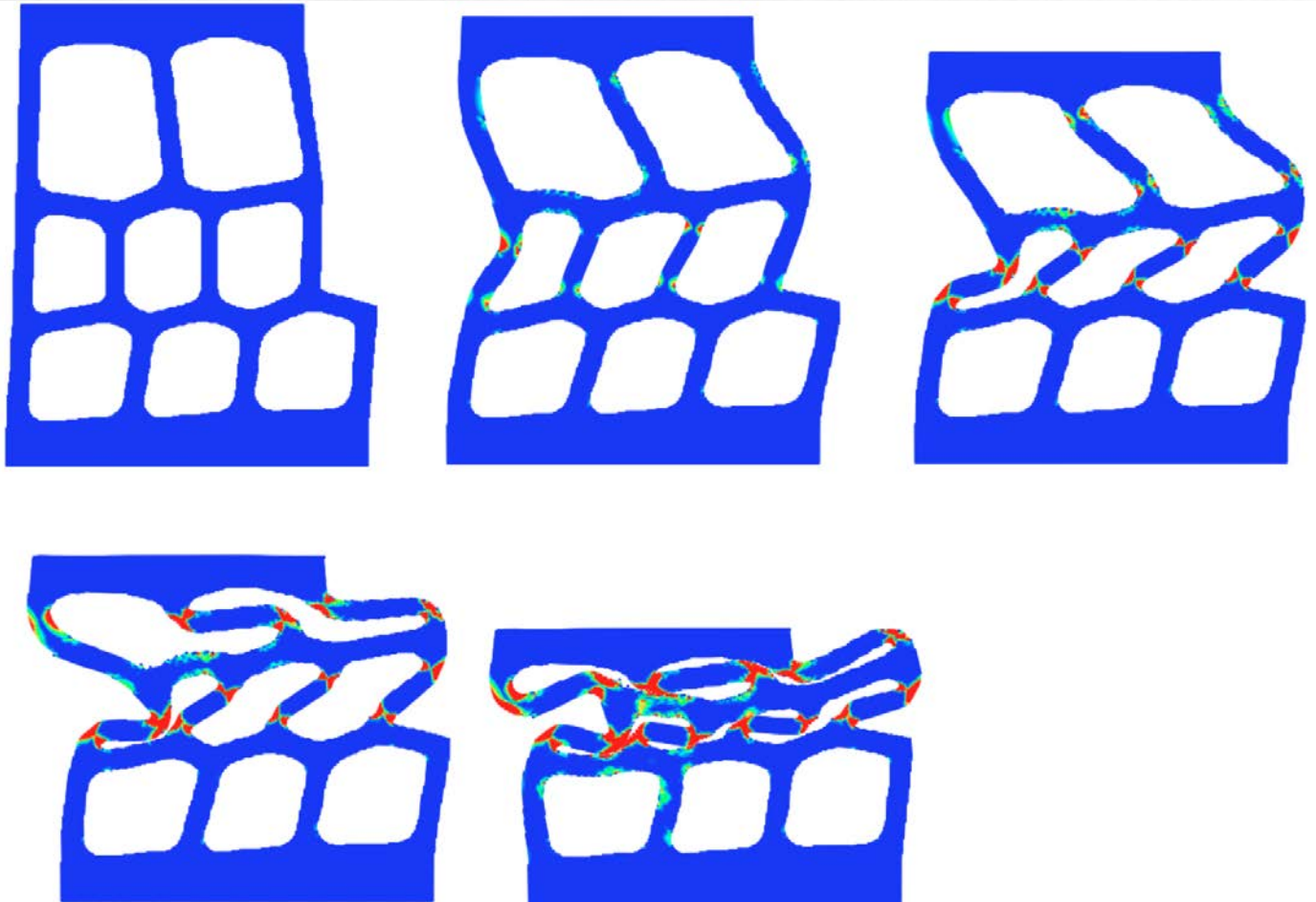
# Cellular material compression

- Comparing **experimental**, **MPM** and **FEM** deformed shapes

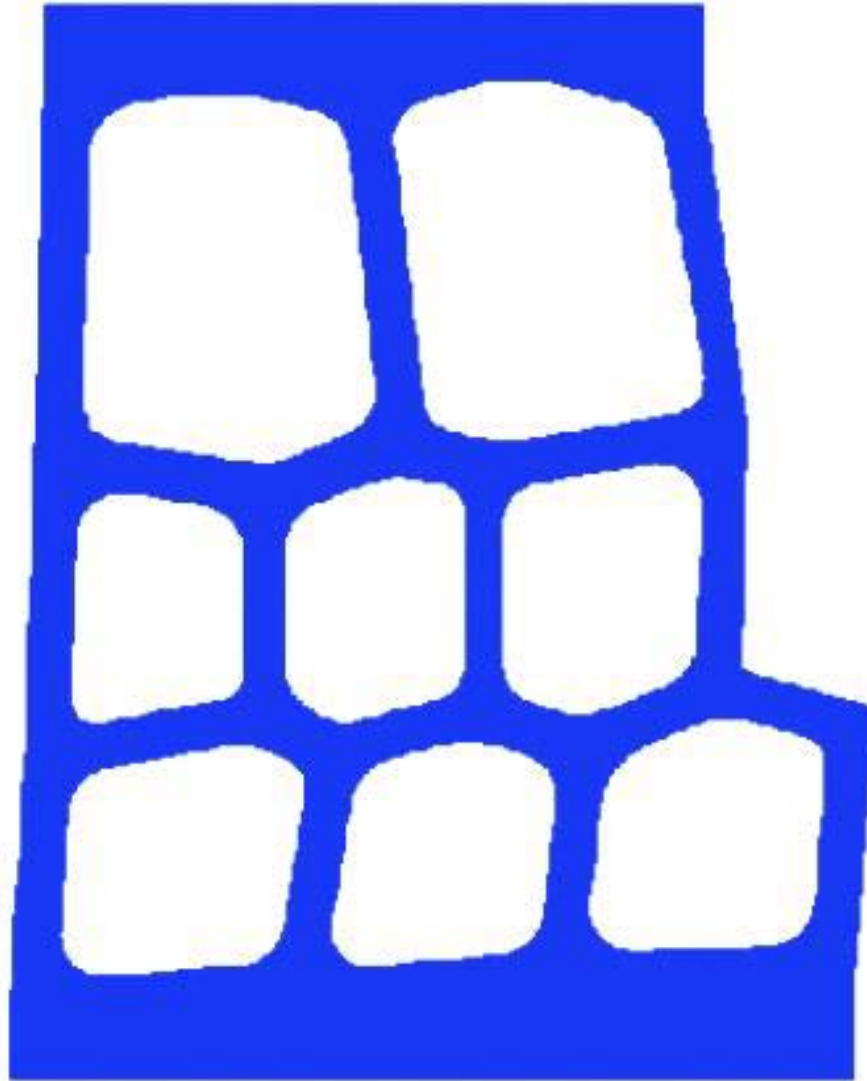
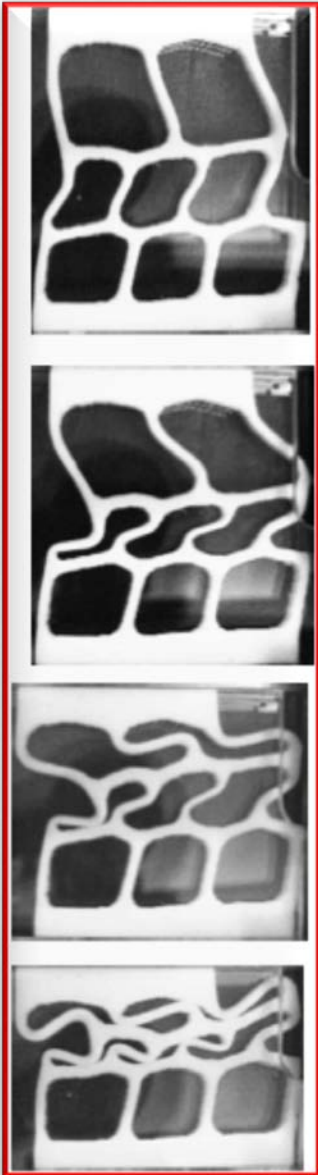


# Cellular material compression – cont'd

- Localization of the cumulative plastic energy in MPM simulations



# Cellular material compression – cont'd



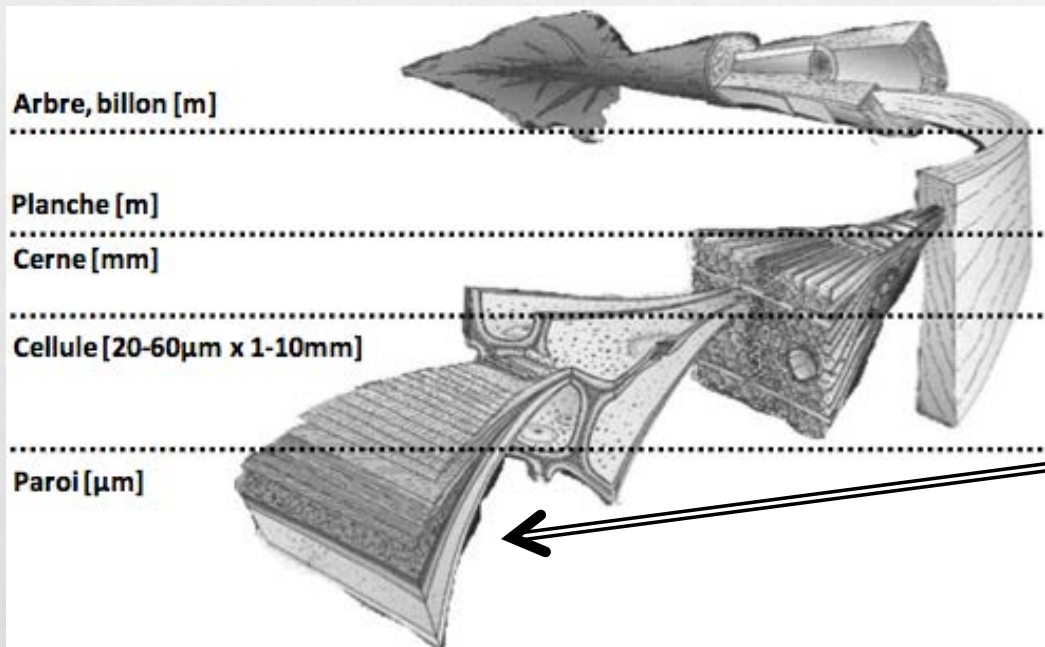
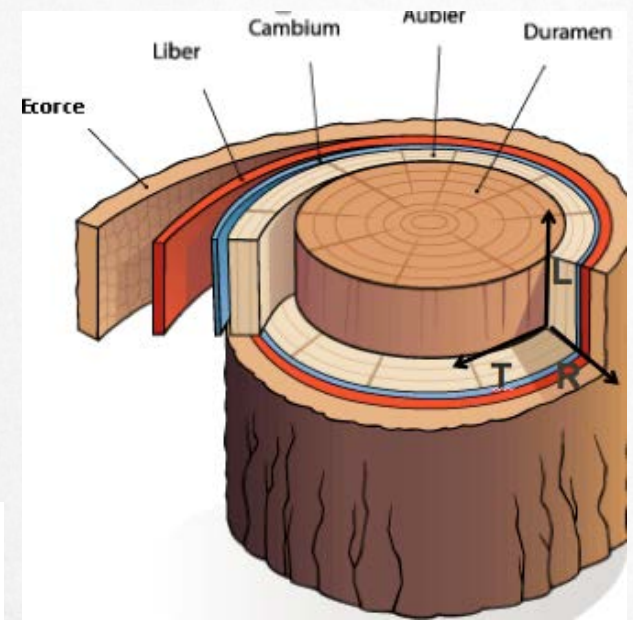
# Outline

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# Wood, a very challenging material

- Wood: a complex material
  - Multiscale,
  - Anisotropic,
  - Composite,
  - ...

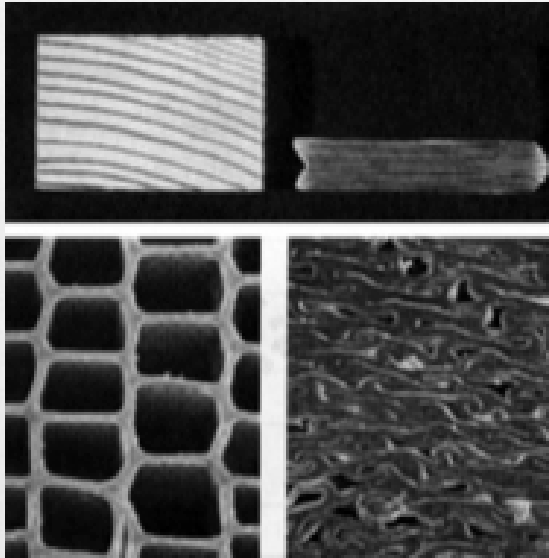


Cell-wall scale :

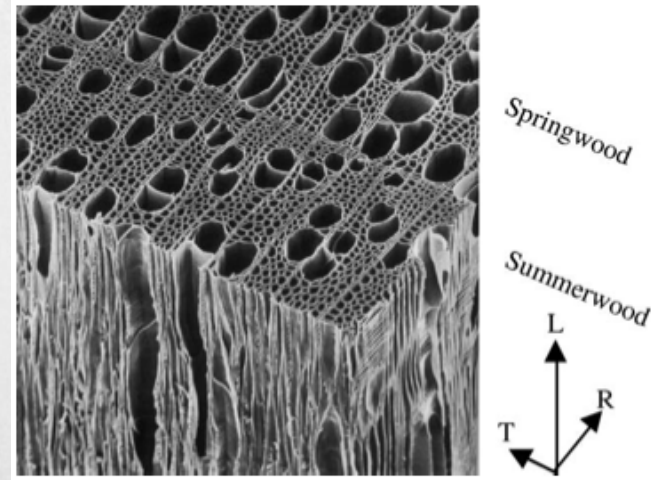
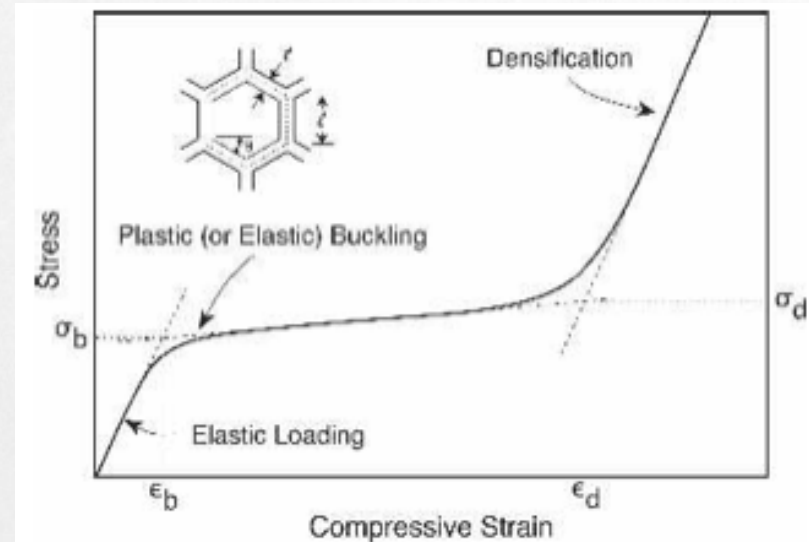
composite material  
(microFiber + matrix)

# Specific wood behavior

- Compression, main deformation of wood processes



Transverse compression  
(Plywood, OSB, etc.)



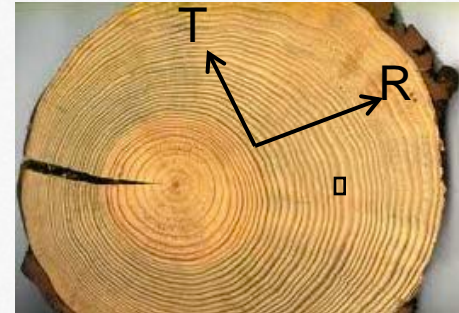
# Transverse wood compression

- Wood properties

- Wood : Loblolly pine

$$E_w = 10.6 \text{ GPa}, \quad \nu_w = 0.33, \quad \rho_w = 1.5 \text{ g/cm}^3$$

$$\sigma_Y = 500 \text{ MPa}, \quad E_p = 0 \text{ MPa}$$

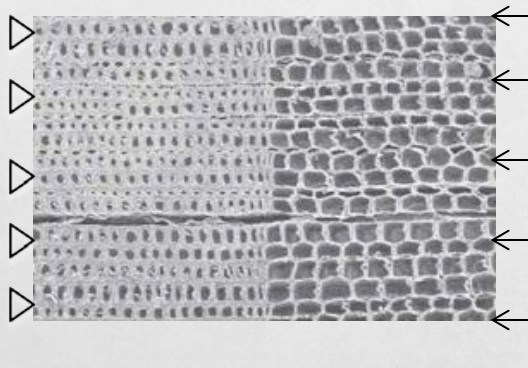


- Micrograph image

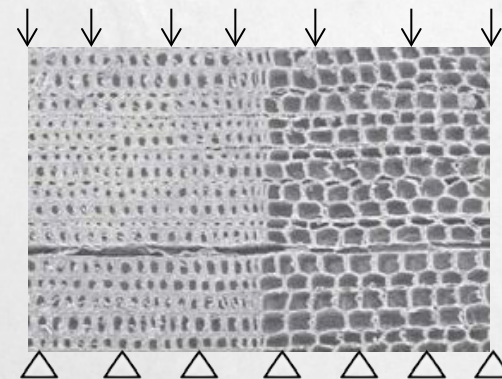
- Micrograph area: : 0.832 x 0.541 mm<sup>2</sup>
- MPM Grid discretization: 300 x 194 elements

- Boundary conditions

Radial compression



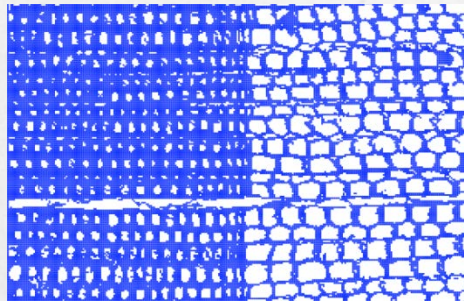
Tangential compression



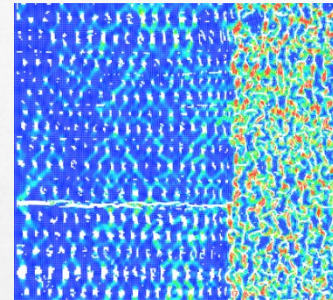


# Radial wood compression

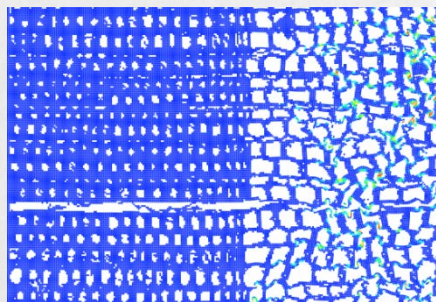
- Localization of plastic zones in the specimen



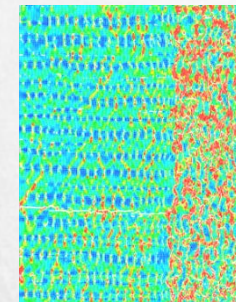
0% cpr



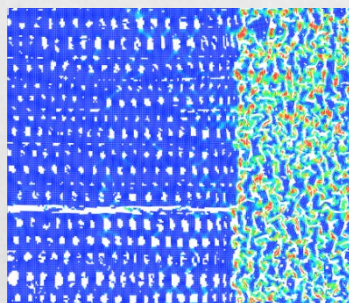
30%



10% cpr



50%



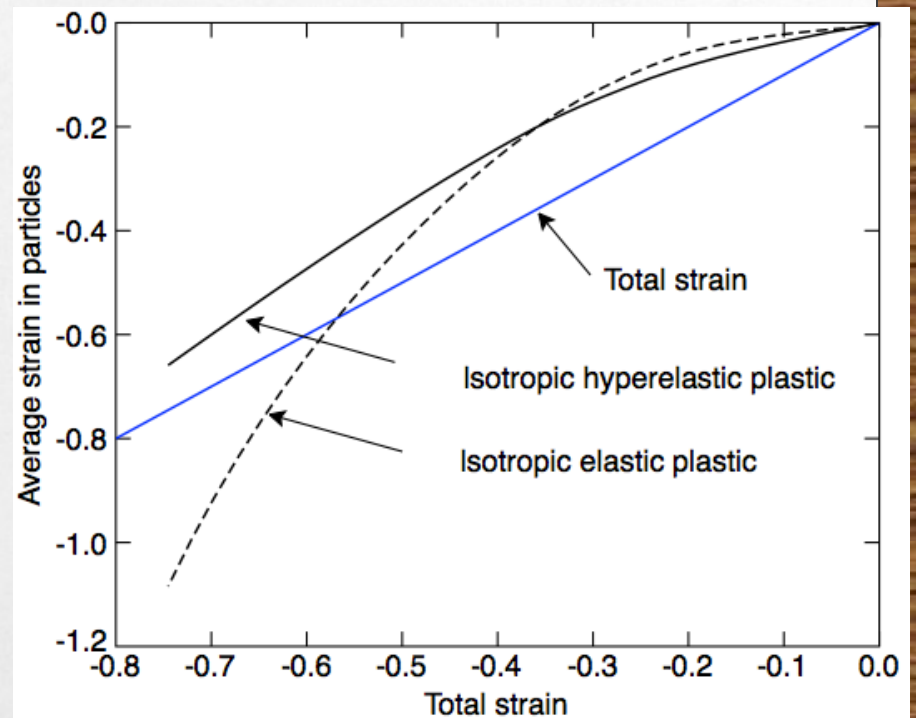
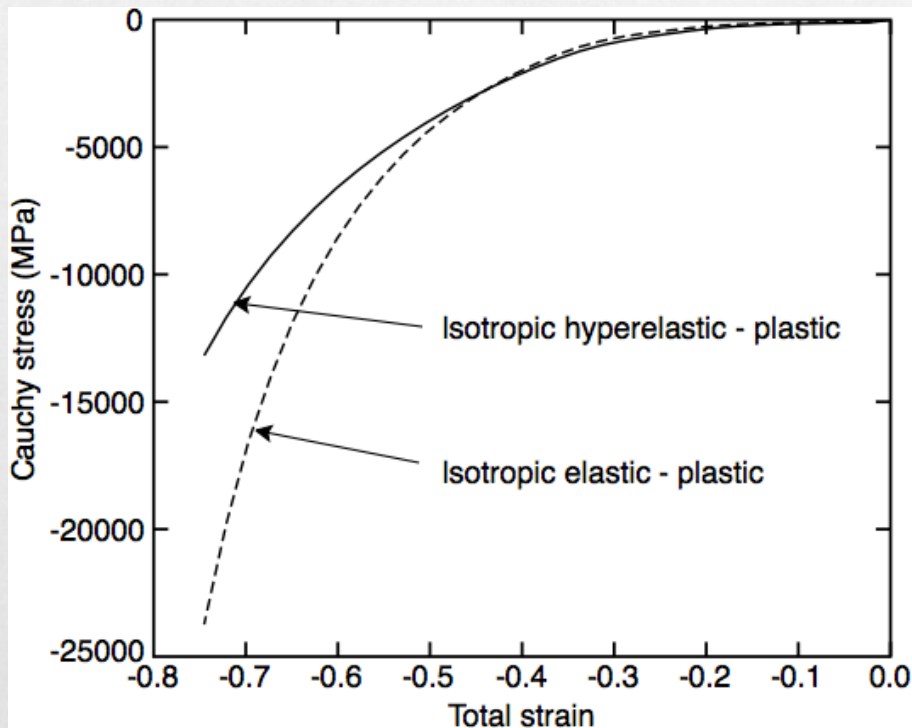
25%



75%

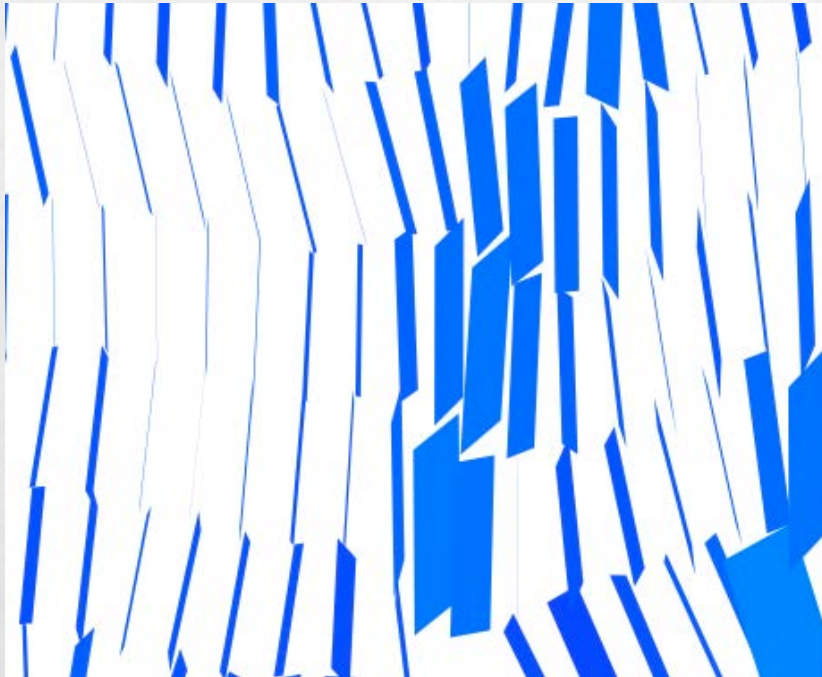
# Radial wood compression – cont'd

- Comparison between models in small and large deformation



# Radial wood compression – cont'd

- Shape of elements at large strains



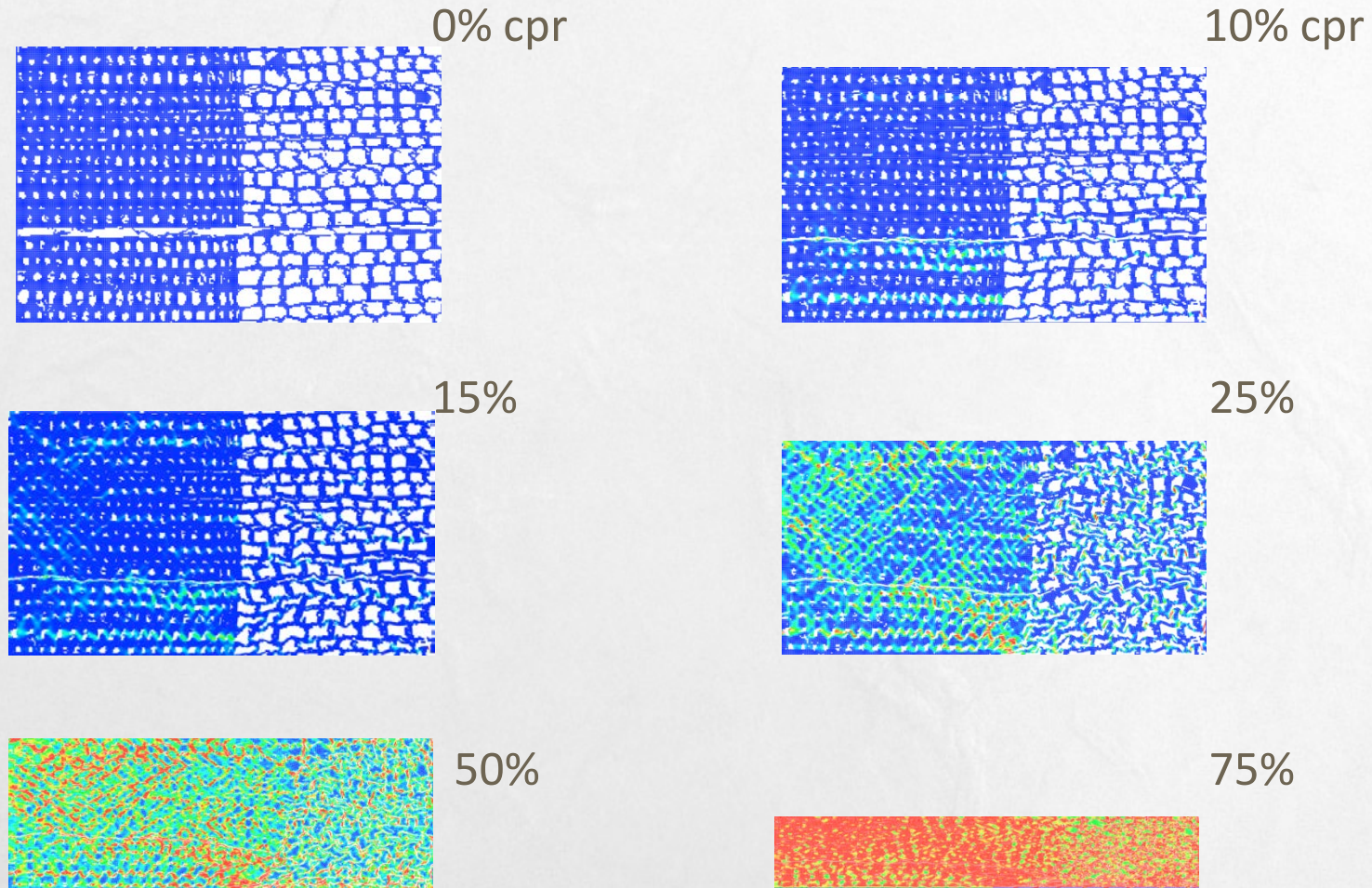
- Small strain model



- Large strain model

# Tangential wood compression

- Localization of plastic energy in the specimen



# Conclusions

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- A hyper elastic-plastic model was successfully implemented in NairnMPM, an MPM software with multiple capabilities
- The hyper elastic-plastic behavior was able to reproduce complex experimental observations seen in wood materials
- The validated hyper elastic-plastic law simulated in MPM allows a better understanding of the distribution of the plastic energy which is critical to many industrial problems

***Thank you !***